

Article title (17/20)
Article title (continued)

Author 1 full name^{a,*}, Author 2 full name^{a,b}, Author 3 full name^b, . . . (13/15)

^aAuthor affiliation 1

^bAuthor affiliation 2

. . . continue with one author affiliation per line (8/10)

Abstract

All text throughout this document is in Times New Roman font. For the purpose of estimating paper length, the formatting of this first page is not critical. Nevertheless, the fonts and line spacings that are used in a *Proceedings of the Combustion Institute* paper are used here, for completeness. The title is 17pt bold, centered, with a line spacing (for multiple-line titles) of 20pt. The authors' names are 13pt, centered, with a line spacing (for cases where the names require more than one line) of 15pt. The affiliations are 8pt italic, centered, with a line spacing of 10pt. Authors are linked to their respective affiliations as indicated above. You can consult a Volume 39 *Proceedings* paper for the information to include in each affiliation. The asterisk denotes the corresponding author. The abstract text is 9pt, justified, with a line spacing of 10pt, and runs the full text width of 5.67 in (144 mm). And the semicolon-separated list of keywords (below the abstract) is 8pt, left-justified, with a line spacing of 10pt. The commands defined in the template conform to these specifications. A typical abstract will fill approximately 15-20 lines. It may appear that there is room to begin the main text at the bottom of the first page. However, in most recently published *Proceedings* papers, the front matter fills the entire first page, or very close to it. The reason is that extensive header and footer material is added in the final published papers. The intent here is that the total paper length as formatted for publication in the *Proceedings* should not exceed eight pages. Therefore, for the purpose of estimating paper length, the main text for all submissions must begin at the top of page 3, following the information that is to be provided by authors on page 2. That leaves seven full pages (pages 3-9) for the text of the paper, including references. This corresponds to an equivalent word count of approximately 6000 words, in the specified two-column format.

Keywords: Keyword 1; Keyword 2; Keyword 3; . . . (8/10)

1. Introduction

Start the main text at top of page 3, using two-column format. The width of each column is 2.67 in (67.7 mm), and the space between the two columns is 0.33 in (8.47 mm). As stated in the Abstract, Times New Roman font is used throughout. Pagewise line numbers are included, to facilitate the review process.

The main text uses 9pt font with the line spacing set to exactly 10pt, and is justified. There are 61 lines per column, including headings and spaces, such that the total height of each column is 8.5 in (216 mm)

There is no extra space between paragraphs. The first line of each new paragraph is indented 0.15 in (3.8 mm).

The formatting definitions specified in the template make minor modifications to the `article.cls` document class to implement the required fonts and line spacing. The 10pt font option is specified initially. The commands `\small` and `\baselineskip 10pt` must be placed after `\begin{document}` to convert to a 9pt font size with 10pt spacing.

2. Sections and subsections

Sections are numbered sequentially using Arabic numerals. Section headings are left-justified, using 10pt bold font, and are followed by a 10pt space.

Subsections are numbered sequentially within each section using Arabic numerals, as indicated below. Subsection headings are left-justified, using 10pt italic font, and are followed by a 10pt space.

For numbered sections, use the `\section`, `\subsection` and `\subsubsection` commands as defined in the template. Include the `\addvspace{10pt}` command after each of the section heading commands.

2.1. Subsection heading

Here is subsection 2.1 text.

2.2. Another subsection heading

If sub-subsections are used, the font and spacing for sub-subsection headings are the same as those for subsection headings, and the numbering is sequential within each subsection. For example, the first sub-subsection for the current subsection would be numbered 2.2.1, the second would be numbered 2.2.2, and so on.

3. Figures, tables, and equations

Figure and tables are to be inserted at the location in which they are expected to appear in the paper. No separate list of figures and tables is to be provided.

Single-column figures (e.g., Fig. 1) should fit within the 2.67 in (67.7 mm) column width. Double-column figures (e.g., Fig. 2) should be sized for legibility, and the image must fit within the 5.67 in

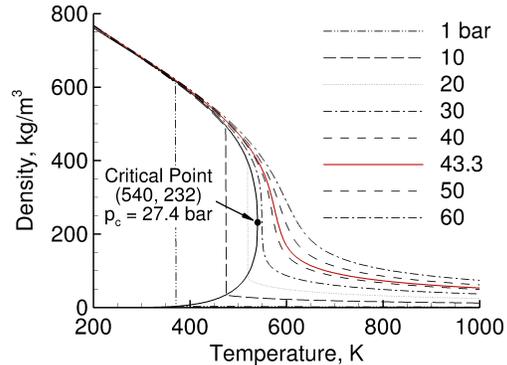


Fig. 1: Density versus temperature of n-heptane.

(144 mm) full text width. Figures are numbered sequentially using Arabic numerals. Figure captions use 8pt font with 10pt spacing.

Single- and double-column tables are inserted similarly. The font size throughout a table is 8pt, with 10pt line spacing. Table 1 is an example of a single-column table, and Table 2 is an example of a double-column table.

Table 1: Engine specifications and operating conditions.

| Description (units) | Value |
|---------------------------------|-------|
| Bore (mm) | 86 |
| Stroke (mm) | 86 |
| Connecting rod (mm) | 159 |
| Geometric compression ratio (-) | 8.9 |
| Engine speed (r/min) | 1300 |
| Intake manifold pressure (kPa) | 95 |
| Global equivalence ratio | 0.2 |

Equations are numbered sequentially in the order in which they appear. Recent *Proceedings* papers can be consulted for appropriate equation formatting. Equation (1) is an example of a numbered equation. The Reynolds number, Re , is defined as:

$$Re \equiv UL/\nu, \quad (1)$$

where U is a characteristic velocity, L is a characteristic length, and ν is the fluid kinematic viscosity.

4. Some example text

The text in this section is taken from [1]. It is included here so that the text will carry over across two more pages. There are no formatting instructions in this section.

Globally fuel-lean, stratified combustion in direct-injection spark-ignition (DISI) engines has the potential to reduce fuel consumption and carbon-dioxide emissions, compared to conventional stoichiometric homogeneous-charge engines. Issues include cycle-to-cycle variations (CCV) and criteria pollutant emissions, which require that the engine be calibrated

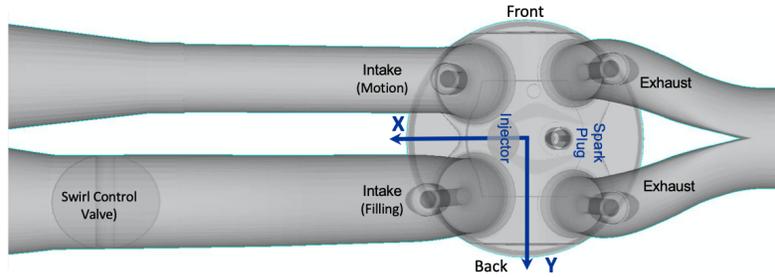


Fig. 2: Engine configuration (top view).

1 to operate at conditions that are suboptimal for efficiency.

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3 CCV have been studied extensively, using both experimental and computational approaches. In the case of homogeneous reactants, it has been shown that the early flame development largely determines the outcome of the combustion event. Most published CCV work has focused on the vicinity of spark plug at the time of ignition and the early flame development.

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10 Spray-guided DISI (SG-DISI) engines operating in stratified mode offer additional complexities. The fuel is injected late, with appropriate timing and targeting to yield a flammable mixture at the spark plug at the time of ignition, and spark timing is limited to a narrow window after the end of injection. Exhaust-gas recirculation (EGR) may be used to control NO_x, leading to even higher levels of CCV. It has been found that misfires in a SG-DISI engine correspond to cases where a flame kernel is initialized by the spark, but the kernel fails to fully develop into a propagating turbulent flame because it is advected away from the flammable mixture. Also, in the absence of in-cylinder fuel injection, in-cylinder turbulence levels increase in direct proportion to engine speed. In contrast, the turbulence level was found to increase by only 30% with a doubling of engine speed in a late-injection SG-DISI engine. This implies that the heat release associated with the main combustion event in a stratified SG-DISI engine is determined by the mixing and turbulence induced by the injection event. In-cylinder swirl has been shown to reduce variability as the engine speed is increased in a SG-DISI engine. Swirl generates a repeatable vortex near the spray centerline, which redistributes momentum, and thus reduces variability, but increases soot formation. Swirl and tumble also can lead to asymmetrical fuel distributions.

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38 The engine is a four-valve, four-stroke-cycle, single-cylinder, optically accessible spark-ignition engine with direct in-cylinder fuel injection (Fig. 2). One intake port has a swirl-control valve that is used to modify the large-scale in-cylinder flow structure. Two of the eight spray plumes straddle the spark plug. The engine can be operated with early fuel injection, or in spray-guided stratified mode with late fuel injection.

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47 Here a globally fuel-lean part-load stratified operating condition is considered, for which experimental results over 350 consecutive cycles are available.

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50 The fuel is an iso-octane/toluene blend; the toluene is included to enable equivalence-ratio measurements. Engine specifications and operating conditions are summarized in Table 1.

54 5. Unnumbered sections

55 The Declaration of competing interest, Acknowledgements, Supplementary material (if included), and References section headings are not numbered. The font and spacing are the same as those for regular section headings.

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60 For references, BibTeX can be used in the usual way. Here the references are provided in the file `PCI_LaTeX.bib`. Several examples of references are included there. Recent *Proceedings* papers can be consulted for details concerning reference citing and formatting. The font size in the References section is 8pt with 10pt line spacing. The `pci.bst` bibliography style file should be used (included in this directory); this is identical to Elsevier's `elsarticle-num.bst`.

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70 Note that titles are to be included for journal articles. In the event that a paper is accepted for publication in the *Proceedings*, links will be added in the final published paper to directly access each of the references, where available. It is not necessary to include such links in your submitted manuscript.

76 6. Nomenclature and appendix

77 A nomenclature section and appendix are rarely included in *Proceedings* papers, because of length limitations. In the event that a nomenclature section is included, it should appear before the first numbered section heading under the unnumbered section heading “Nomenclature.”

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82 If an appendix is included, it should appear immediately before the references under the unnumbered section heading “Appendix.”

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89 The formatting for these section headings should be the same as that used for the Declaration of competing interest, Acknowledgements, Supplementary material, and References.

90 Declaration of competing interest

91 This is a required section, in which authors are to disclose any competing interests relating to the work

Table 2: Chemical mechanisms for multicomponent fuels.

| First author | Fuels or molecules | # of species /# of reactions | Validation cases | Reference | Mechanism designation |
|---------------|--------------------|---------------------------------|---------------------|-----------|--------------------------|
| O. Abianeh | TRF-Ethanol | 62 / 194 | LFS | [2] | A62 |
| H. Wang | TRF-PAH | 109 / 543 | LFS, HCCI, DICI | [3] | W109 |
| J.C.G. Andrae | TRF-Ethanol | 143 / 672 | LFS, HCCI | [4] | A143 |
| J.C.G. Andrae | TRF-Ethanol | 1121/4961 | ST | [5] | A1121 |

1 reported in the paper. See [6] for Elsevier’s policy.
 2 Authors will be required to complete a form related
 3 to competing interests at the time of manuscript sub-
 4 mission. An appropriate statement in the case of no
 5 competing interests to report is given in the following
 6 paragraph.

7 The authors declare that they have no known com-
 8 peting financial interests or personal relationships that
 9 could have appeared to influence the work reported in
 10 this paper.

11 Use the acknowledgement environment defined in
 12 the template for this section, not `\section*`.

13 Acknowledgments

14 This LaTeX template was updated from the Vol-
 15 ume 39 template by Dan Haworth in July 2023. It
 16 is based on a template that had been created by Joe
 17 Oefelein for earlier *Proceedings* volumes. Figure 1
 18 was taken from that source. Page layout details were
 19 taken from information provided by Joe Oefelein and
 20 Rob Barlow. Figure 2 and Table 1 were provided by
 21 Samuel Kazmouz from [1], and Table 2 is based on a
 22 table from Jun Han’s Ph.D. dissertation [7].

23 Use the acknowledgement environment defined in
 24 the template for this section, not `\section*`.

25 Supplementary material

26 If supplementary material is submitted along with
 27 the manuscript, that should be noted here. In the event
 28 that the manuscript is accepted for publication in the
 29 *Proceedings*, a DOI link to the online supplementary
 30 material will be included in the published paper.

31 Use the acknowledgement environment defined in
 32 the template for this section, not `\section*`.

33 References

- 34 [1] S. J. Kazmouz, D. C. Haworth, P. Lillo, V. Sick, Large-
 35 eddy simulations of a stratified-charge direct-injection
 36 spark-ignition engine: Comparison with experiment and
 37 analysis of cycle-to-cycle variations, *Proc. Combust.*
 38 *Inst.* 38 (2021) 5859–5857.
- 39 [2] O. S. Abianeh, Development of a new skeletal chemical
 40 kinetic mechanism for ethanol reference fuel, *J. Eng.*
 41 *Gas Turb. Pow.* 137 (6) (2015) 061501.
- 42 [3] H. Wang, M. Yao, Z. Yue, M. Jia, R. D. Reitz, A reduced
 43 toluene reference fuel chemical kinetic mechanism for
 44 combustion and polycyclic-aromatic hydrocarbon pre-
 45 dictions, *Combust. Flame* 162 (6) (2015) 2390–2404.
- 46 [4] J. C. Andrae, R. Head, HCCI experiments with gasoline
 47 surrogate fuels modeled by a semidetalled chemical ki-
 48 netic model, *Combust. Flame* 156 (4) (2009) 842–851.

- 49 [5] J. C. Andrae, Development of a detailed kinetic model
 50 for gasoline surrogate fuels, *Fuel* 87 (10-11) (2008)
 51 2013–2022.

- 52 [6] Elsevier, FACTSHEET: Competing Interests,
 53 [https://www.elsevier.com/_data/assets/
 54 pdf_file/0007/653884/Competing-Interests-
 55 factsheet-March-2019.pdf](https://www.elsevier.com/_data/assets/pdf_file/0007/653884/Competing-Interests-factsheet-March-2019.pdf) (2019; accessed
 56 July 2023).

- 57 [7] J. Han, CFD Modeling of Ignition and Soot Formation
 58 for Advanced Compression-Ignition Engines, Ph.D.
 59 Thesis, The Pennsylvania State University, University
 60 Park, PA, USA (2022).